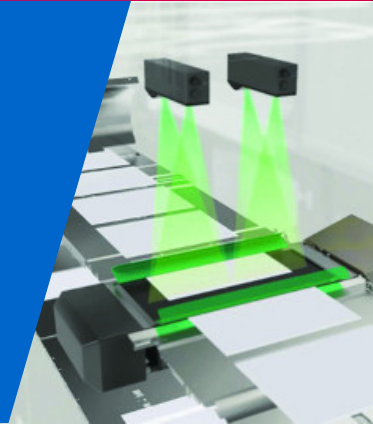


Sensorless Field-Oriented Estimation of Hybrid Stepper Motors in High-Performance Paper Handling

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Where innovation starts

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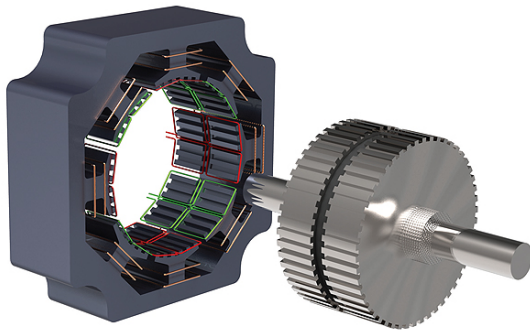


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Hybrid stepper motor (HSM)

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- ▶ **Two-phase HSMs used in direct-drive for printing applications**
- ▶ **Microstepping allows precise positioning**



Problem formulation

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Open-loop control

- ▶ No feedback required
- ▶ Mechanical resonances
- ▶ Ohmic and iron losses $\rightarrow$ heat generation

Problem formulation

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Open-loop control

- ▶ No feedback required
- ▶ Mechanical resonances
- ▶ Ohmic and iron losses → heat generation

Sensorless Field-Oriented control (FOC)

- ▶ Requires feedback
- ▶ Significantly less mechanical vibration
- ▶ Efficient
- ▶ More flexibility (torque control, field-weakening)

Problem formulation

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Research question

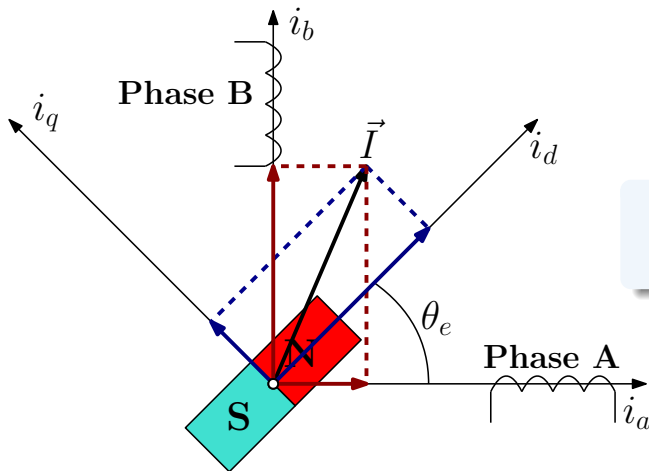
How can sensorless field-oriented control of a hybrid stepper motor be designed and implemented in high-performance paper handling?

Main criteria

- ▶ Achieve rotor position error < 3 electrical degrees (< 1 mrad mechanically)
- ▶ Operation range from 0 RPM to 700 RPM

How to model HSM: choice of reference frames

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$ab\text{-frame} \xrightarrow{\text{park}} dq\text{-frame}$
 $ab\text{-frame} \xleftarrow{\text{inv. park}} dq\text{-frame}$

How to model HSM: in rotating reference frame

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HSM model in rotating reference frame

$$L \frac{di_d}{dt} = v_d - Ri_d + LN(\omega_m i_q)$$

$$L \frac{di_q}{dt} = v_q - Ri_q - LN(\omega_m i_d) - K_m \omega_m$$

$$J \frac{d\omega_m}{dt} = \tau_{em} - B\omega_m - \tau_L$$

$$\frac{d\theta_m}{dt} = \omega_m$$

How to model HSM: in rotating reference frame

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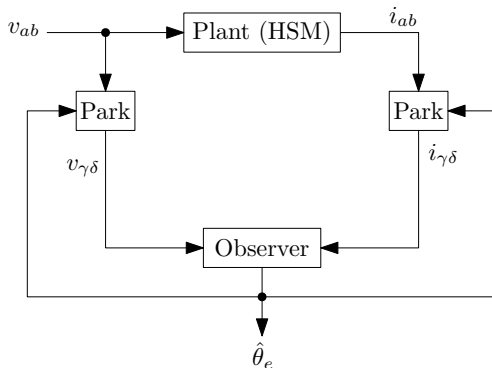
$$\frac{d\theta_m}{dt} = \omega_m$$

Electromagnetic torque is proportional to i_q

$$\tau_{em} = K_m i_q$$

Estimator Design: Luenberger observer in rotor frame

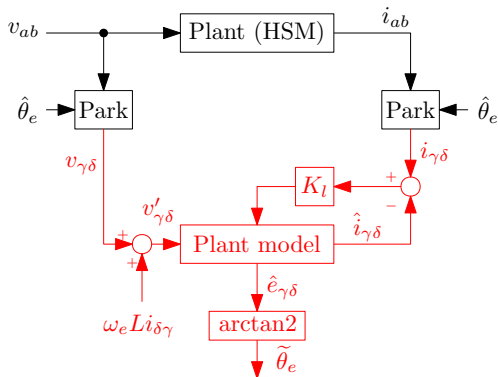
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- Transform observer to rotating frame
- Observed back EMF is DC (at constant speed)

Estimator Design: Luenberger observer in rotor frame

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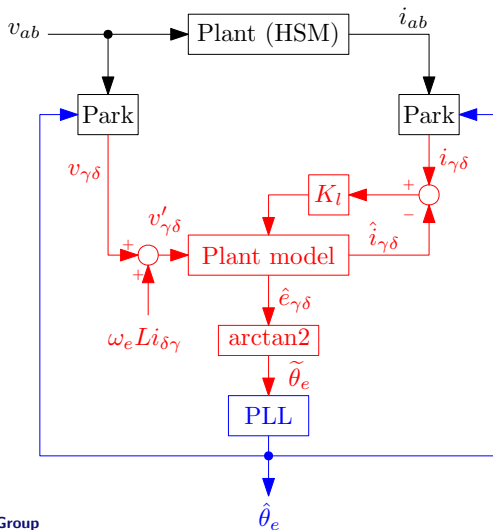


► Transform observer to rotating frame

► Observed back EMF is DC (at constant speed)

Estimator Design: Luenberger observer in rotor frame

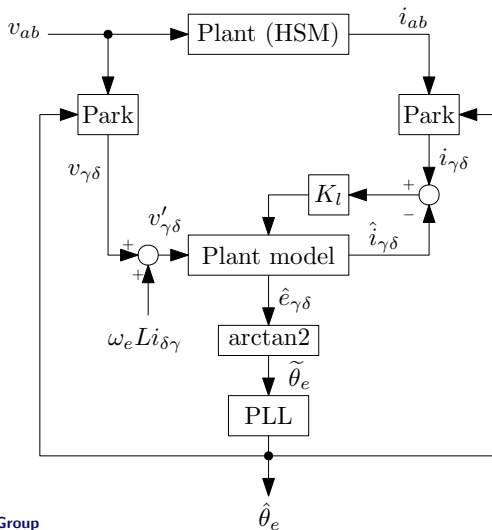
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Estimator Design: Luenberger observer in rotor frame

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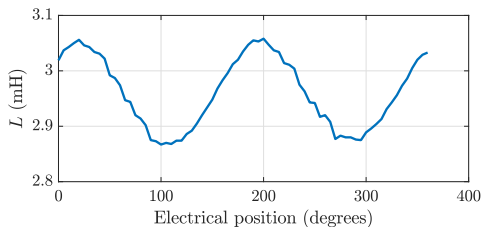


- Transform observer to rotating frame
- Observed back EMF is DC (at constant speed)

Low-speed estimator: saliency-based tracking

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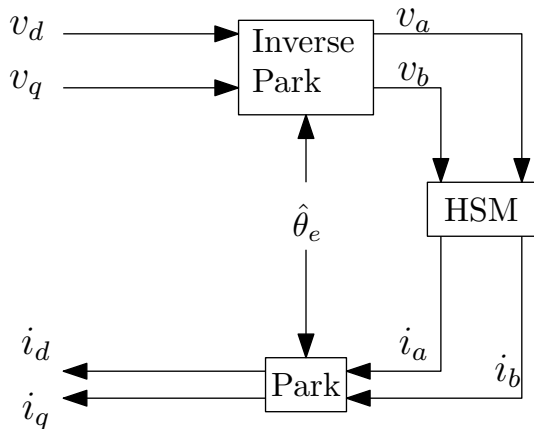
► Phase inductance dependent of rotor position: Saliency



Inject high-frequent signal to obtain rotor position

Low-speed estimator: saliency-based tracking

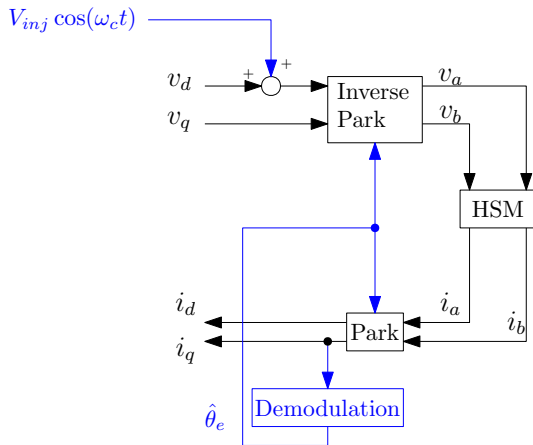
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- ▶ Injection into d -axis to minimize torque ripple
- ▶ Retrieve rotor information from q -axis

Low-speed estimator: saliency-based tracking

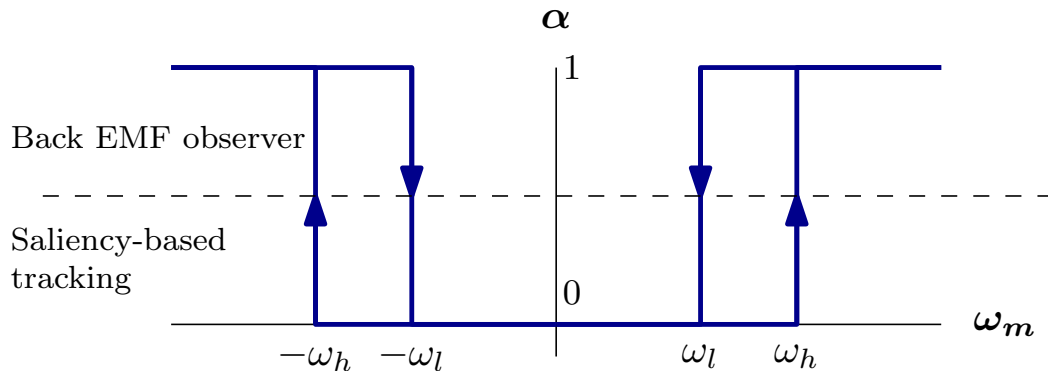
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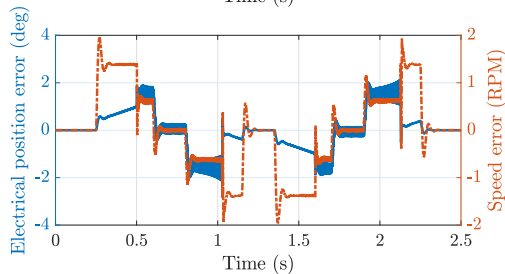
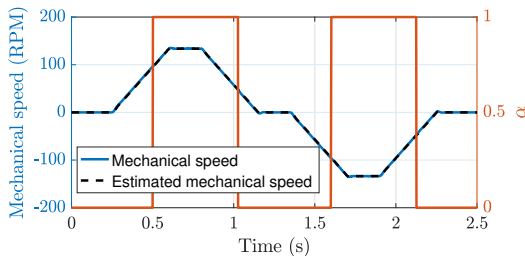
Combining the estimators: switching with hysteresis

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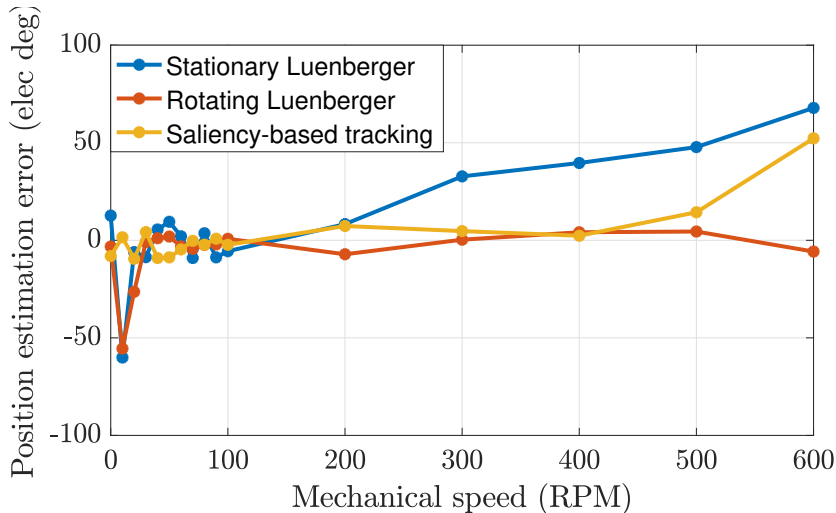
Simulation: Combining the estimators

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Mean error of different estimators

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Experimental results

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- ▶ Rotating Luenberger observer max average error: 7 elec. degrees (mid-to-high speed)
- ▶ Saliency-based tracking max average error: 9 elec. degrees
- ▶ Max speed: 660 RPM

Conclusions

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Sensorless FOC can be designed and implemented for the HSM in high-performance paper handling by dividing the design in several stages

- ▶ HSM modeled in dq -frame for FOC design
- ▶ Position control realized with cascade control
- ▶ Rotating Luenberger observer designed for mid-to-high
- ▶ Saliency-based tracking designed for zero-to-low speed
- ▶ Switching rule with hysteresis to combine estimators

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Recommendations and future work

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Recommendations for experimental setup

- ▶ Use dual H-bridge inverter configuration instead of a three-leg inverter
- ▶ Investigate saliency-based tracking closed-loop issues

Future work for sensorless FOC

- ▶ Extend control structure (Feed-forward, Field-weakening)
- ▶ Investigate observer performance under high load
- ▶ Switch between position control and torque control
- ▶ Analyze performance with paper handling setpoints

Thank You!